

REMARKS

This Preliminary Amendment cancels, without prejudice, original claims 1 to 13 in the underlying PCT Application No. PCT/DE01/01470. The Preliminary Amendment also adds new claims 14 to 26. The new claims conform the claims to U.S. Patent and Trademark Office rules and do not add new matter to the application.

In accordance with 37 C.F.R. § 1.121(b)(3), the Substitute Specification (including the Abstract, but without the claims) contains no new matter. The amendments reflected in the Substitute Specification (including Abstract) are to conform the Specification and Abstract to U.S. Patent and Trademark Office rules or to correct informalities. As required by 37 C.F.R. § 1.121(b)(3)(iii) and § 1.125(b)(2), a Marked Up Version Of The Substitute Specification comparing the Specification of record and the Substitute Specification also accompanies this Preliminary Amendment. Approval and entry of the Substitute Specification (including Abstract) are respectfully requested.

The underlying PCT Application No. PCT/DE01/01470 includes an International Search Report, dated November 29, 2001, a copy of which is submitted herewith. The Search Report includes a list of documents that were considered by the examiner in the underlying PCT application.

Applicants assert that the subject matter of the present application is new, non-obvious, and useful. Prompt consideration and allowance of the application are respectfully requested.

Respectfully Submitted,

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[10191/2301]

SHEATHED ELEMENT GLOW PLUG HAVING AN
IONIC CURRENT SENSOR AND A METHOD OF OPERATING
SUCH A SHEATHED ELEMENT GLOW PLUG

[Background Information

] FIELD OF THE INVENTION

The present invention relates to a ceramic sheathed element
glow plug for diesel engines having an ionic current sensor
5 [according to the definition of the species of the first
independent claim]. [Unexamined] German Published Patent
Application No. 34 28 371 [has already described] describes
ceramic sheathed element glow plugs having a ceramic heating
element. The ceramic heating element has an electrode made of
10 a metallic material which is used to determine the electric
conductivity of the ionized gas present in the combustion
chamber of the internal combustion engine. The wall of the
combustion chamber functions as the second electrode.

15 In addition, there are also [known] conventional sheathed
element glow plugs having a housing in which is situated a
rod-shaped heating element in a concentric bore. The heating
element here is composed of at least one insulation layer and
a first feeder layer and a second feeder layer, the first and
20 second feeder layers being connected by a web at the tip of
the heating element on the combustion chamber end. The
insulation layer is made of an electrically insulating ceramic
material, and the first and second feeder layers as well as
the web are made of an electrically conducting ceramic
25 material.

[Advantages of the Invention

] SUMMARY OF THE INVENTION

[The] A ceramic sheathed element glow plug according to the
30 present invention having the ionic current sensor [with the

features of the first independent claim has the advantage that the sheathed element glow plug having the ionic current sensor has] may include a very simple design and [is] may be inexpensive to manufacture. [It is also advantageous that]
5 Furthermore, the expansion coefficients of the individual layers [are] may be matched to one another.

Advantageous refinements of and improvements on the sheathed element glow plug having the ionic current sensor
10 [characterized in the main claim are possible through] may be possible. According to one example embodiment of the [measures characterized in the subclaims. A design of a] sheathed element glow plug [which is especially advantageous from a design standpoint may be achieved if the feeder layers], the
15 feeder layers may function as an electrode for detecting [the] an ionic current. [It is advantageous if the electric] Electric terminals of the feeder layers [are] may be provided on the end of the heating element remote from the combustion chamber so that operation of the sheathed element glow plug as
20 an ionic current sensor [becomes possible. It is also advantageous to additionally provide] may become possible. Additionally an ionic current detection electrode may be provided which runs inside the insulation layer or is applied to the insulation layer because in this [way] manner glow
25 operation and ionic current measurement may [take place] occur simultaneously. [It has proven advantageous here for the] The ionic current detection electrode [to] may be arranged laterally on the surface on the combustion chamber-side end of the heating element to thus [guarantee] ensure a sufficient
30 distance between the feeder layer and the ionic current detection electrode. [It is also advantageous for the] The ionic current detection electrode [to be continued] may continue to the end of the heating element on the combustion chamber side, because in this [way] manner it [is] may be
35 possible to detect an ionic current in an area of the

combustion chamber which [is] may be important for the combustion processes [taking place] occurring in the combustion chamber. [It is furthermore advantageous to use the] Furthermore, a ceramic composite structure [described below] (described below) may be used for the various layers of the heating element whose conductivity and expansion coefficient [are very highly] may be adaptable. This [is] may likewise be true of the precursor composite materials described below.

[It is furthermore advantageous for the] The sheathed element glow plug having the ionic current sensor [to] may be operated according to different methods. [It is advantageous for ionic] Ionic current detection [to take place] may occur, for example, in a different time window than the glow phase, because this [permits] may permit accurate ionic current detection. [It is also advantageous to provide the] The ionic current detection may occur during the glow phase of the heating element, because it [is interesting] may be desirable to also detect the combustion process in the startup phase of the internal combustion engine.

[Additional advantages are derived from the following description of the embodiments.

Brief Description of the Drawing

Embodiments of the present invention are illustrated in the drawing and are explained in greater detail in the following description.

] BRIEF DESCRIPTION OF THE DRAWINGS

Fig. 1 shows] Fig. 1 is a schematic diagram of an example embodiment of a sheathed element glow plug according to the present invention having an ionic current sensor in a longitudinal section[.,].

Fig. 2 [shows] is a schematic diagram of [the] an example embodiment of a combustion chamber-side end of a sheathed element glow plug according to the present invention having an ionic current sensor in a longitudinal section[,].

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Fig. 3 [shows] is a schematic diagram of an example embodiment of a heating element of a sheathed element glow plug according to the present invention having an ionic current sensor in cross section[,].

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Fig. 4 [shows] is a schematic diagram of an end remote from the combustion chamber in another example embodiment of the sheathed element glow plug according to the present invention having an ionic current sensor in longitudinal section[, and].

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Figs. 5 and 6 each [show] illustrate a schematic longitudinal section through a combustion chamber-side end of a heating element of a sheathed element glow plug according to the present invention having an ionic current sensor.

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[Description of the Embodiments] DETAILED DESCRIPTION

Fig. 1 [shows] is a schematic diagram of a longitudinal section through a sheathed element glow plug according to an example embodiment the present invention. A tubular housing 3, [preferably] which may be, for example, made of metal, holds a heating element 5 in its concentric bore on the combustion chamber-side end. Heating element 5 is made of a ceramic material. Heating element 5 has a first feeder layer 7 and a second feeder layer 9, first feeder layer 7 and second feeder layer 9 being made of an electrically conducting ceramic material. On end 6 of the heating element remote from the combustion chamber, first feeder layer 7 and second feeder layer 9 are connected by a web 8 which is also made of an electrically conducting ceramic material. First feeder layer 7 and second feeder layer 9 are separated by an insulation layer

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11. Insulation layer 11 is made of an electrically insulating ceramic material. The interior of housing 3 is sealed in the direction of the combustion chamber by a combustion chamber seal 13 surrounding heating element 5 in a ring. On the end of heating element 5 remote from the combustion chamber, first feeder layer 7 is connected to a first terminal 15. This first terminal 15 is in turn connected to terminal stud 19 in the direction of the end of the sheathed element glow plug remote from the combustion chamber. Second feeder layer 9 is connected at its end remote from the combustion chamber to a second terminal 17 which passes through terminal stud 19 and continues to the end of the sheathed element glow plug remote from the combustion chamber, second terminal 17 being electrically insulated from the terminal stud. Terminal stud 19 is kept at a distance from the end of heating element 5 remote from the combustion chamber by a ceramic spacer sleeve 27 situated in the concentric bore of housing 3. In the direction of the end remote from the combustion chamber, terminal stud 19 passes through a tension sleeve 29 and a metal sleeve 31. On the end of the sheathed element glow plug remote from the combustion chamber, a round plug 25 is attached to terminal stud 19, establishing the electric connection. The end of the concentric bore of housing 3 remote from the combustion chamber is sealed and electrically insulated by a hose ring 21 and an insulation disc 23.

In this example embodiment the sheathed element glow plug [is] may be operated so that the sheathed element glow plug is first operated in the heating mode in starting up the internal combustion engine. This means that during the glow phase, a positive voltage is applied to first terminal 15 and a negative voltage is applied to second terminal 17 or vice versa, so that a current flows across first feeder layer 17, web 8 and second feeder layer 9. The electric resistance along this path raises the temperature of the heating element and the combustion chamber into which the end of the sheathed

element glow plug on the combustion chamber side protrudes, and thus the plug is heated. Heating element 5 is glazed on its end remote from the combustion chamber beyond the combustion chamber edge of housing 3, so that there is no electric contact between first or second feeder layers and housing 3.

After the end of the glow phase, the same high voltage potential is applied to first terminal 15 and second terminal 17 so that no more current flows in the feeder layers, but first feeder layer 7 and second feeder layer 9 function as the ionic current measurement electrode. If the combustion chamber is ionized by the presence of ions, an ionic current may flow from the ionic current detection electrode, i.e., from first feeder layer 7 and second feeder layer 9, to the wall of the combustion chamber which is at ground. Thus in this example embodiment, first feeder layer 7 and second feeder layer 9 function as an ionic current detection electrode.

Fig. 2 illustrates schematically another example embodiment of a sheathed element glow plug according to the present invention having an ionic current sensor in a longitudinal section. In this case only the combustion chamber-side end of such a sheathed element glow plug is [shown] illustrated. The end of this sheathed element glow plug remote from the combustion chamber corresponds to the [design] configuration in the example embodiment [according to] illustrated in Fig. [11] 1. Heating element 5 is again arranged in a concentric bore in housing 3, which [is preferably] may be made of metal. Heating element 5 is again composed of a first feeder layer 7, a second feeder layer 9 and an insulation layer 11, the cross section of heating element 5 [shown] illustrated in this diagram being cut in a plane so that only insulation layer 11 is visible (this plane is perpendicular to the section plane of Fig. 1). Insulation layer 11 and first feeder layer 7, web 8 and second feeder layer 9 are again made of materials which

were already mentioned in conjunction with Fig. 1. First feeder layer 7 is connected to a terminal stud 19 by a first terminal 15. Terminal stud 19 is again kept at a distance from the end of the heating element which is remote from the combustion chamber by a ceramic spacer sleeve 27. The combustion chamber-side sealing of the interior of metallic housing 3 is again accomplished by a combustion chamber seal 13, which, in this example embodiment, is made of an electrically conducting material because the second feeder layer is connected to ground via combustion chamber seal 13 to housing 3. A glazing applied on the outside to the surface of the first feeder layer in the area of housing 3 and combustion chamber seal 13 prevents first feeder layer 7 from contacting combustion chamber seal 13 and housing 3.

In this example embodiment, an ionic current detection electrode 33, running from the end of heating element 5 remote from the combustion chamber to tip 6 of heating element 5 near the combustion chamber, is provided in insulation layer 11. Ionic current detection electrode 33 runs laterally on the surface of heating element 5 at tip 6 on the combustion chamber side. Ionic current detection electrode 33 is made of an electrically conducting ceramic material or a metallic material. The end of the ionic current detection electrode which is remote from the combustion chamber is connected to a second terminal 17 which runs through terminal stud 19 to the end of the sheathed element glow plug remote from the combustion chamber.

Fig. 3 [shows] illustrates a cross section through heating element 5, illustrating the arrangement of terminals in the individual layers of the heating element again in detail. The cross section shows an area on the end of heating element 5 remote from the combustion chamber. First terminal 15 is connected to first feeder layer 7 while second terminal 17 is connected to the ionic current detection electrode which runs

through insulation layer 11. In addition, second feeder layer 9 which has electric contact via electrically conducting combustion chamber seal 13 to housing 3, which is at ground, is also [shown] illustrated in an area situated further in the direction of the combustion chamber.

[This embodiment has an especially great advantage inasmuch as] In this example embodiment, the sheathed element glow plug may be operated in glow operation and as an ionic current detection device simultaneously. To do so, the voltage required for glow operation is applied to first feeder layer 7 via terminal stud 19 and first terminal 15, and the voltage required for ionic current detection is applied to ionic current detection electrode 33 via second terminal 17.

Fig. 4 illustrates another example embodiment of a sheathed element glow plug having an ionic current sensor. By analogy with Fig. 3, the combustion chamber-side end of such a sheathed element glow plug is illustrated schematically in a longitudinal section. Heating element 5 is also [shown] illustrated sectioned in a plane in which only insulation 11 is visible, as in Fig. 2. The same reference numbers in this figure and in the following figures denote the same parts as in the preceding figures; therefore, they will not be discussed again here.

An ionic current detection electrode 33 again passes through the insulation layer, but this electrode extends to the outermost combustion chamber-side tip 13 of heating element 5. In contrast with the example embodiment illustrated in Fig. 2, the electrode does not continue laterally beyond the surface of the heating element. Since ionic current detection electrode 33 now passes centrally through insulation layer 11, the connection to first terminal 17 is also centrally situated. In [a preferred] an example embodiment, first terminal 17 passes through a spring element 35 situated in a

concentric bore in spacer sleeve 27, which [is preferably] may
be insulated from spring element 35, and continuing through
terminal 19 in the direction of the end of the sheathed
element glow plug remote from the combustion chamber. Spring
5 element 35 makes it possible to apply pressure to heating
element 5 or terminal stud 19 and establishes the electric
contact with first feeder layer 7, so that optimal electric
contact and optimal sealing of the interior of housing 3 from
the environment may be achieved by combustion chamber seal 13.
10 The interior of housing 3 is sealed via spacer sleeve 27. The
electric contact of second feeder layer 9 is [designed]
configured like that in the embodiment described on the basis
of Fig. 2.

15 In another example embodiment, the terminals remote from the
combustion chamber on first feeder layer 7 and on ionic
current detection electrode 33 may also be [designed]
configured without spring element 35 by analogy with Fig. 2.

20 On the basis of Figs. 5 and 6, various example embodiments of
the [design] configuration of combustion chamber-side tip 6 of
heating element 5 are [shown] depicted for the example
embodiment illustrated in Fig. 4. Each [shows] illustrates a
longitudinal section through the combustion chamber-side tip
25 of heating element 5.

Fig. 5 illustrates ionic current detection electrode 33 which
runs to the combustion chamber-side tip of heating element 5
within insulation layer 11, which extends to combustion
30 chamber-side tip 6 of heating element 5. First feeder layer 7
and second feeder layer 9 are connected by web 8 in only two
areas, which are [situated] arranged at a distance from the
area in which ionic current detection electrode 33 extends up
to combustion chamber-side tip 6 of the heating element 8 in
35 the radial direction (with respect to the longitudinal axis

through heating element 5, i.e., through the sheathed element glow plug). Fig. 5 also [shows] illustrates that in [a preferred] an example embodiment, the ionic current detection electrode [is situated] may be arranged in an insulation sleeve 36 which extends almost to the combustion chamber-side end of the sheathed element glow plug.

Fig. 6 shows another example embodiment in which ionic current detection electrode 33 continues laterally to combustion chamber-side tip 6 of heating element 5, and combustion chamber-side end 6 of heating element 5 has only one area in which first feeder layer 7 and second feeder layer 9 are connected by a web 8. The area in which web 8 is [arranged] configured in this example embodiment is [situated] arranged on the side of combustion chamber-side tip 6 of heating element 5 which does not have ionic current detection electrode 33. In this example embodiment, the sheathed element glow plug [is preferably situated] may be arranged in the combustion chamber, so that the side of combustion chamber-side tip 6 of heating element 5 on which web 8 is [situated] configured projects the greatest distance into the combustion chamber. This [should] may be taken into account in particular in an arrangement when the sheathed element glow plug projects obliquely into the combustion chamber.

The example embodiment illustrated on the basis of Figs. 4, 5 and 6 [preferably] may include an ionic current detection electrode made of an electrically conducting ceramic material.

In another variant of the example embodiments illustrated on the basis of Figs. 2 through 6, ionic current detection electrode 33 may also be applied externally to insulation layer 11.

As mentioned above, the materials of first feeder layer 7, web 8, second feeder layer 9, insulation layer 11 and ionic current detection electrode 33 [should] may be made of a ceramic material. This [guarantees] may ensure that the thermal expansion coefficients of the materials [will] may hardly differ at all, thus virtually guaranteeing the long-term stability of heating element 5. The material of first feeder layer 7, web 8 and second feeder layer 9 is selected so that the resistance of these layers is less than the resistance of insulation layer 11. Likewise, the resistance of first ionic current detection electrode 33 is less than the resistance of insulation layer 11.

In [a preferred] an example embodiment, first feeder layer 7, web 8 and second feeder layer 9, insulation layer 11 and first electrode 33 are made of ceramic composite structures containing at least two of the compounds Al_2O_3 , MoSi_2 , Si_3N_4 and Y_2O_3 . These composite structures are obtainable by a sintering operation in one or two steps. The specific resistance of the layers may be determined [preferably], for example, on the basis of the MoSi_2 content and/or the core size of MoSi_2 , the MoSi_2 content of first feeder layer 7, web 8 and second feeder layer 9 as well as first ionic current detection electrode 33 [preferably being] may be higher than the MoSi_2 content of insulation layer 11.

In example another embodiment, first feeder layer 7, web 8 and second feeder layer 9, insulation layer 11, and first ionic current detection electrode 33 are made of a precursor ceramic having different filler contents. The matrix of this material [is composed of] includes polysiloxanes, [polysequioxanes] polysilsesquioxanes, polysilanes or polysilazanes which may be doped with boron, nitrogen or aluminum and are produced by pyrolysis. At least one of the compounds Al_2O_3 , MoSi_2 , SiO_2 and SiC forms the filler for the individual layers. By analogy

with the composite structure described above, the MoSi_2 content and/or the grain size of MoSi_2 may [preferably] determine the resistance of the layers. The MoSi_2 content of first feeder layer 7, web 8 and second feeder layer 9 as well as first ionic current detection electrode 33 [is preferably] may be higher than the MoSi_2 content of insulation layer 11. In the example embodiments described above, the compositions of first feeder layer 7, web 8, second feeder layer 9, insulation layer 11 and first ionic current detection electrode 33 are selected so that their thermal expansion coefficients and the shrinkage that [occurs] may occur during the sintering and pyrolysis process are the same, so that no cracks develop in heating element 5.

